

Downstream Etching of Parylene-N Films

Russell Callahan

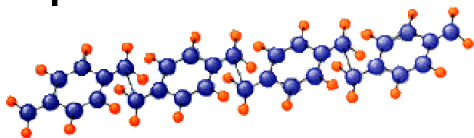
Gregory Raupp

Stephen Beaudoin

Arizona State University

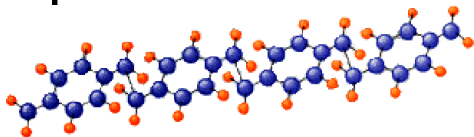
Department of Chemical, Bio, and Materials Engineering

Tempe, AZ 85287-6006



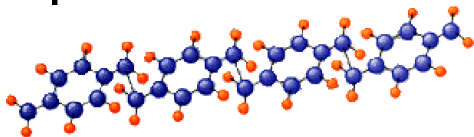
Significance of Research

- Performance advantage
 - Parylene's lower dielectric constant, relative to silicon dioxide, offers increased performance
- Environmental advantage
 - Use of oxygen plasma as the dielectric etchant gas eliminates the need for perfluorinated compounds(PFCs) in IC manufacturing
 - ⇒ PFCs are undesirable greenhouse gases



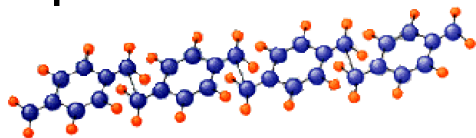
Research Goals

- Characterize downstream etching of parylene-n
 - Investigate effects of process variables on etch performance
 - Temperature
 - Pressure
 - Plasma power
 - Total gas flow
 - Develop experimentally-validated transport and reaction models

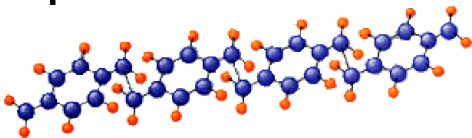
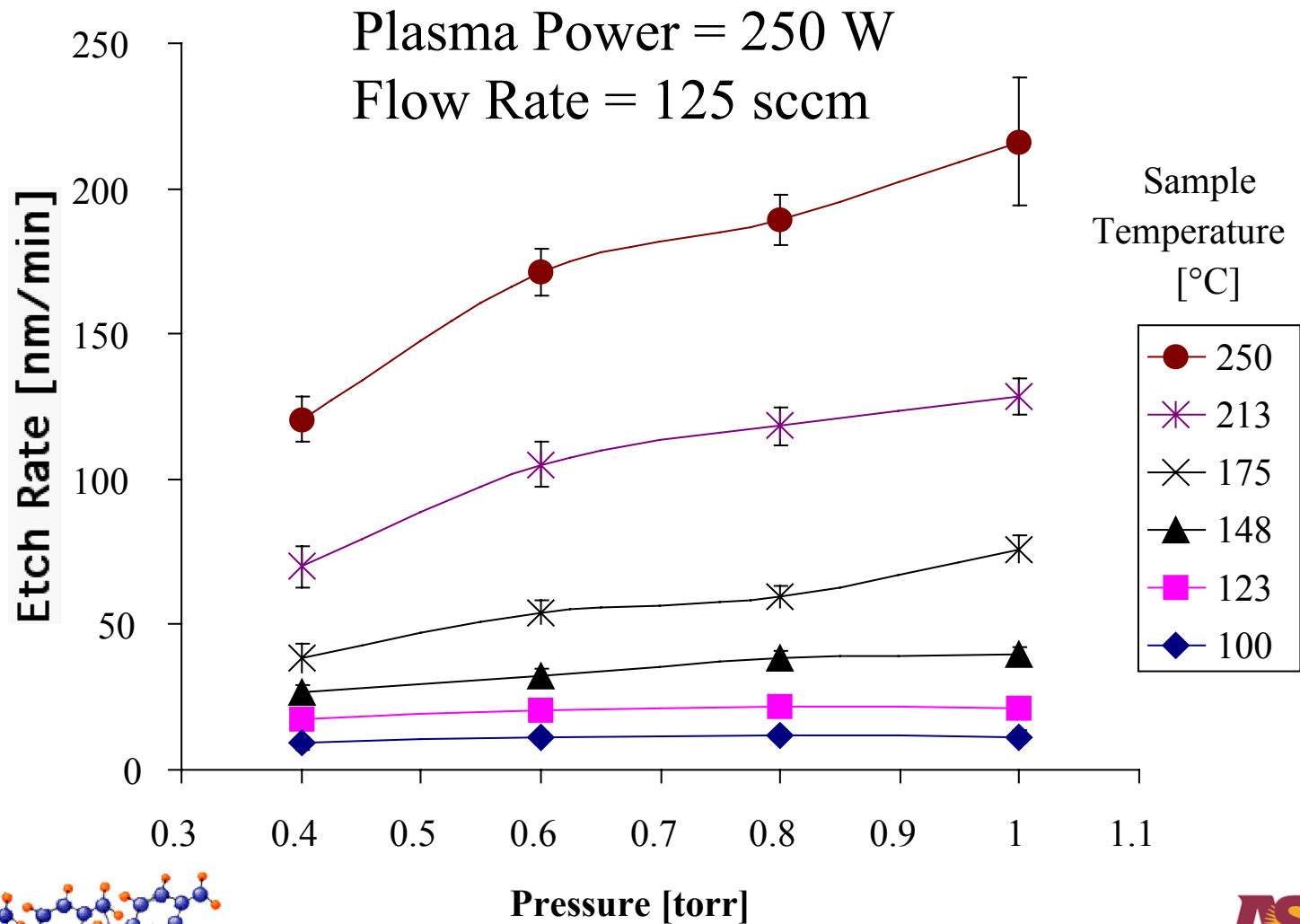


Downstream Etching Apparatus

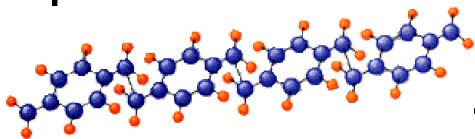
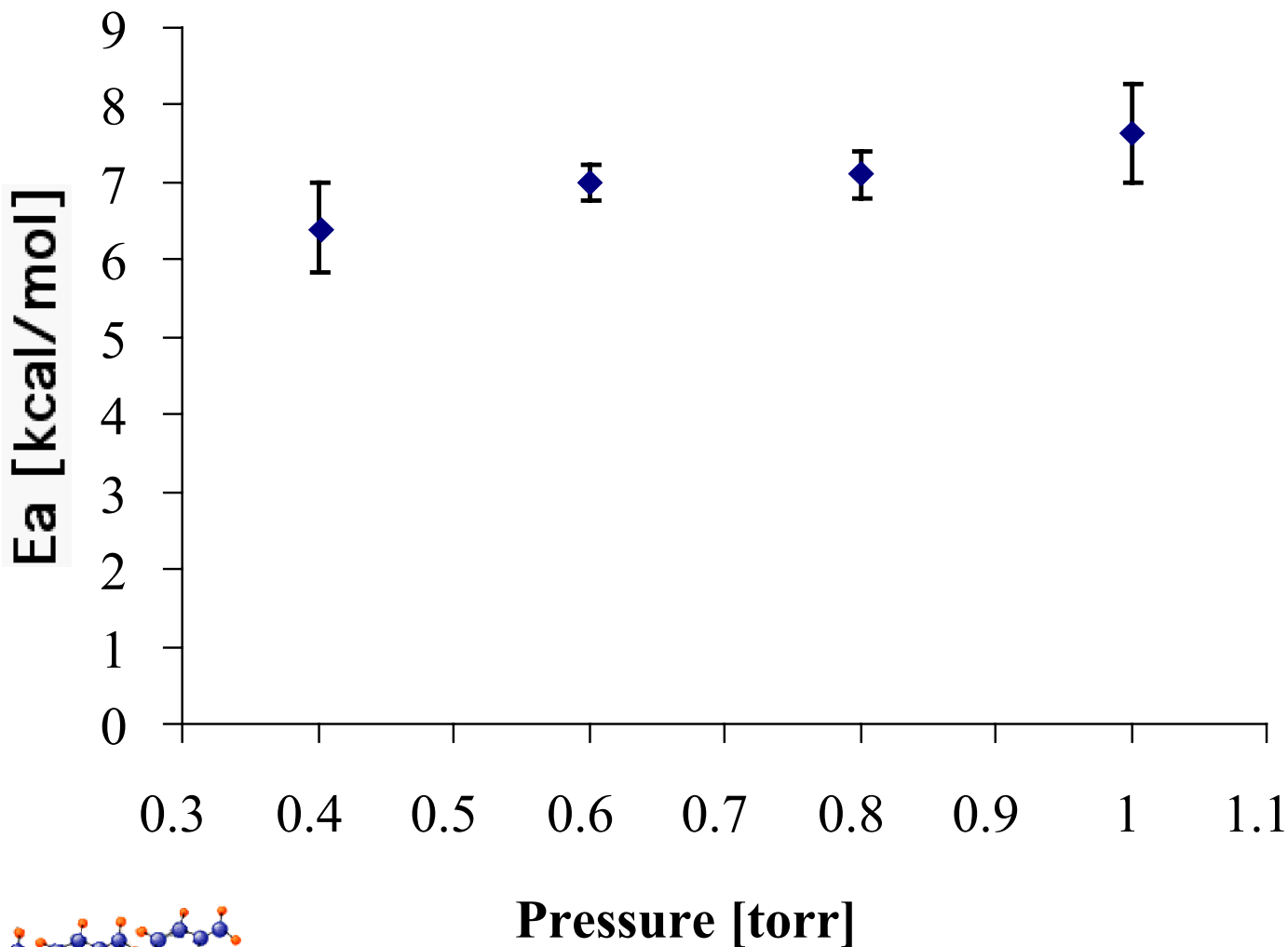
- 250 W Astex microwave generator to create downstream oxygen plasma
- Base pressure = 4×10^{-7} Torr
- Temperature controlled substrate holder



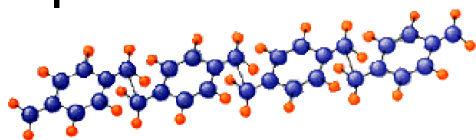
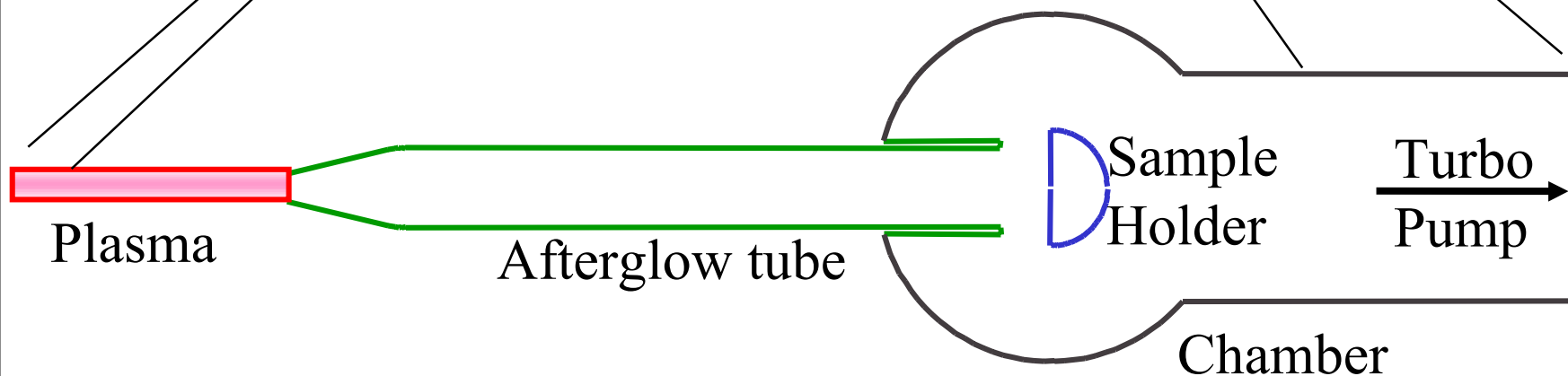
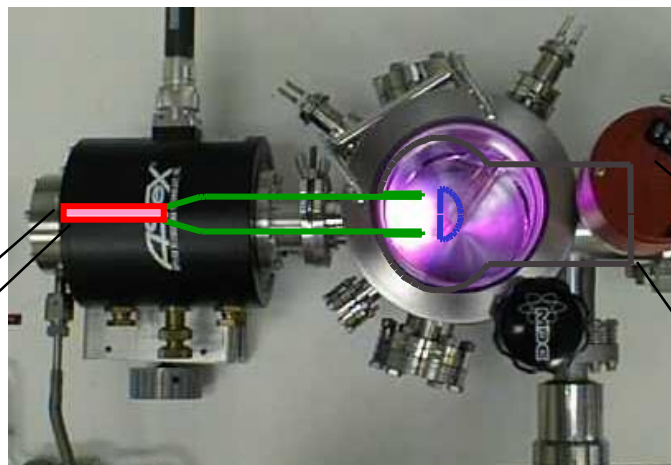
Experimental Results: Etch Rate as a Function of Temperature and Pressure



Apparent Activation Energy



Modeling: System Geometry

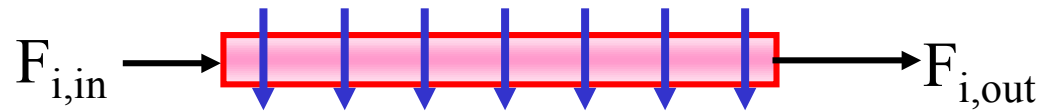


Plasma Model

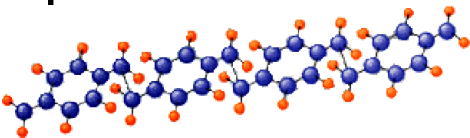
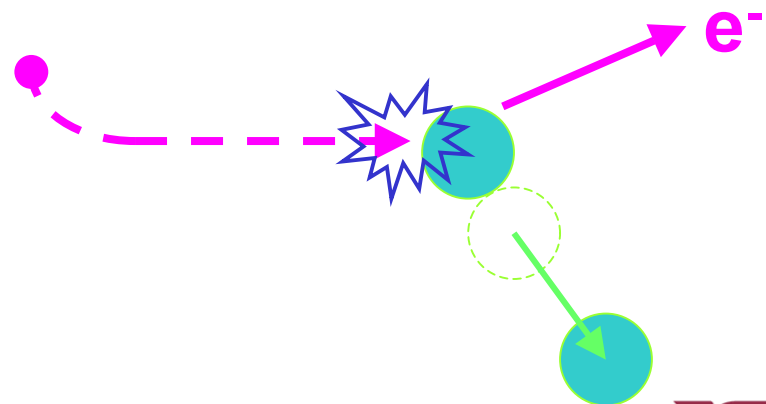
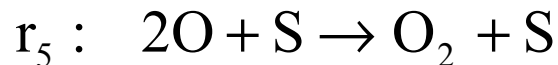
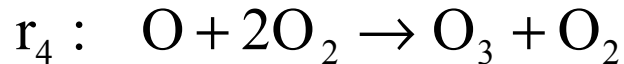
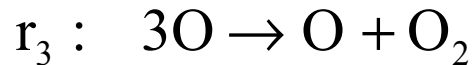
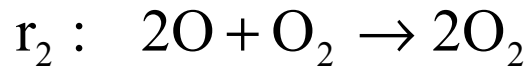
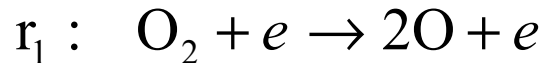
- CSTR reactor

- Assumes uniform microwave intensity

$$F_{i,in} = F_{i,out} + (-r_i)V$$

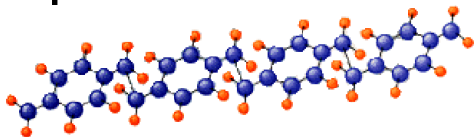


- Generation and recombination reactions

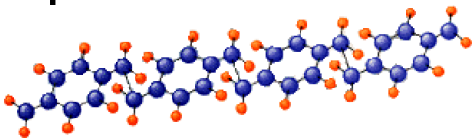
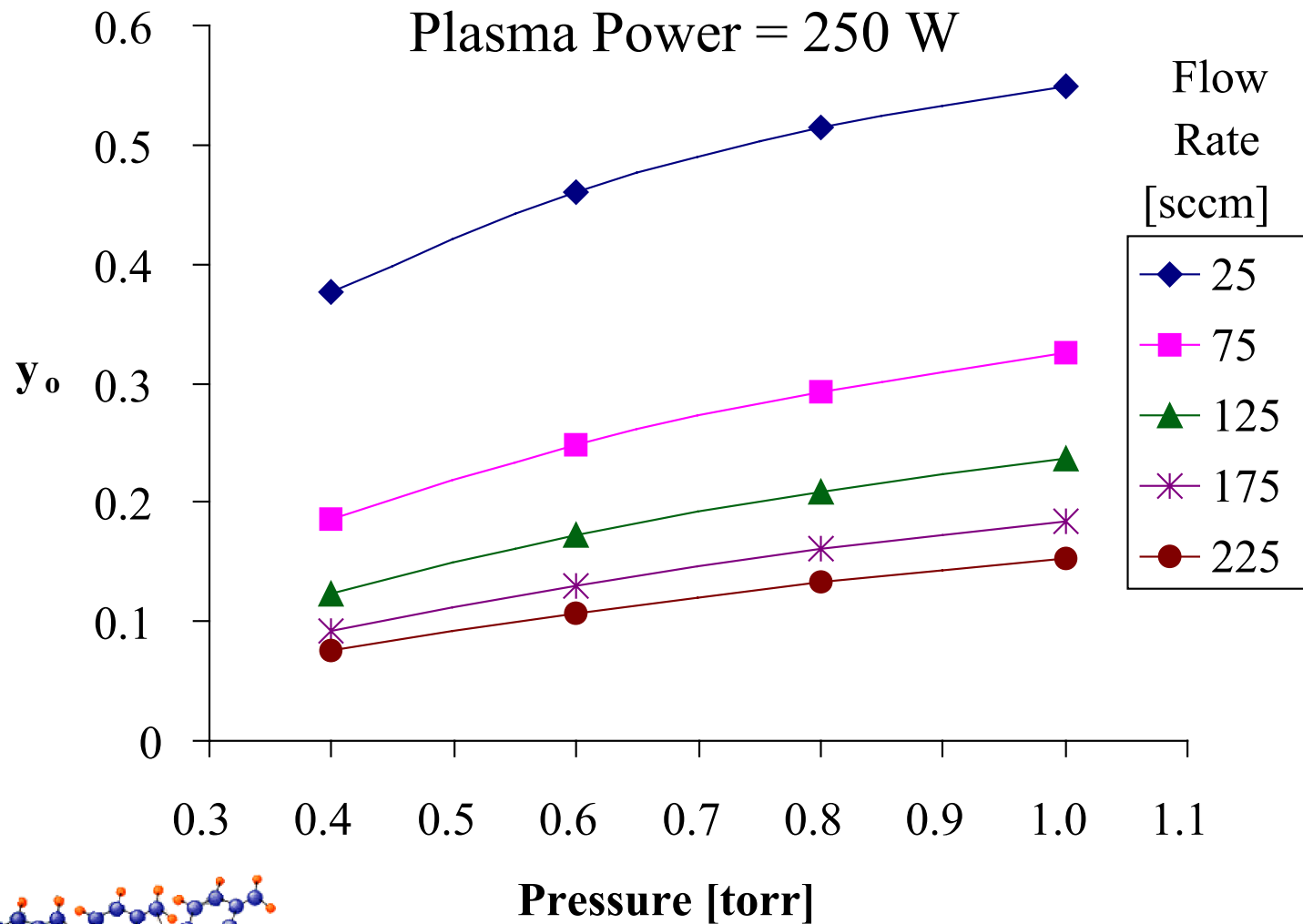


Plasma Model

- Rate constants taken from literature
- Four equations;
 - three species balances
 - molar balance ($\sum y_i = 1$)
- Used result as a boundary condition for the transport model



Results: Atomic Oxygen Mole Fraction as a Function of Pressure and Flow Rate



Transport Model

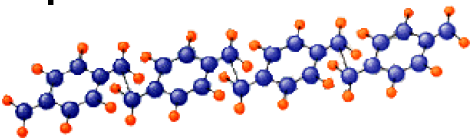
- Dimensionless quantities

$$v_r^* = \frac{v_r}{V}, v_z^* = \frac{v_z}{V}, z^* = \frac{z}{D}, r^* = \frac{r}{D}, y_o = \frac{n_o}{N}, P^* = \frac{(P - P_o)}{\rho V^2}$$

- Dimensionless momentum equations

$$\text{Re} \left(v_r^* \frac{\partial v_z^*}{\partial r^*} + v_z^* \frac{\partial v_z^*}{\partial z^*} \right) = \frac{1}{r^*} \frac{\partial}{\partial r^*} \left(r^* \frac{\partial v_z^*}{\partial r^*} \right) + \frac{\partial^2 v_z^*}{\partial z^{*2}} - \text{Re} \frac{\partial P^*}{\partial z^*}$$

$$\text{Re} \left(v_r^* \frac{\partial v_r^*}{\partial r^*} + v_z^* \frac{\partial v_r^*}{\partial z^*} \right) = \frac{\partial}{\partial r^*} \left(\frac{1}{r^*} \frac{\partial}{\partial r^*} (r^* v_z^*) \right) + \frac{\partial^2 v_r^*}{\partial z^{*2}} - \text{Re} \frac{\partial P^*}{\partial r^*}$$



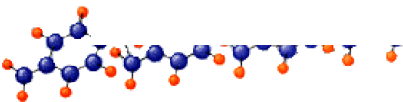
Transport Model, con't

- Dimensionless mass balance

$$\left(\frac{1}{r^*} \frac{\partial}{\partial r^*} r^* \frac{\partial y_o}{\partial r^*} + \frac{\partial^2 y_o}{\partial z^{*2}} \right) - \text{Pe} \left(v_r^* \frac{\partial y_o}{\partial r^*} + v_z^* \frac{\partial y_o}{\partial z^*} \right) - 2\text{Da}_2 y_o^2 (1 - y_o) - 2\text{Da}_3 (y_o)^3 - \text{Da}_4 y_o (1 - y_o)^2 = 0$$

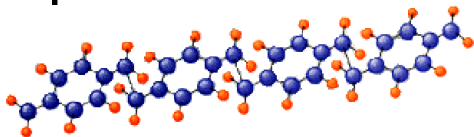
- Pressure distribution

$$\frac{\partial^2 P^*}{\partial z^{*2}} + \frac{\partial^2 P^*}{\partial r^{*2}} = \frac{v_z^*}{r^*} \frac{\partial v_r^*}{\partial z^*} + \frac{v_r^*}{r^*} \frac{\partial v_z^*}{\partial r^*} + \frac{1}{\text{Re} r^*} \frac{\partial}{\partial r^*} \left(\frac{\partial v_z^*}{\partial z^*} \right) - \left(\left(\frac{v_r^*}{r^*} \right)^2 + \left(\frac{\partial v_z^*}{\partial z^*} \right)^2 + \left(\frac{\partial v_r^*}{\partial r^*} \right)^2 + \frac{1}{\text{Re} r^*} \frac{\partial^2 v_r^*}{\partial z^{*2}} + 2 \frac{\partial v_r^*}{\partial z^*} \frac{\partial v_z^*}{\partial r^*} \right) + \text{Constant} \cdot \left(\frac{1}{r^*} \frac{\partial}{\partial r^*} (r^* v_r^*) + \frac{\partial v_z^*}{\partial z^*} \right)$$



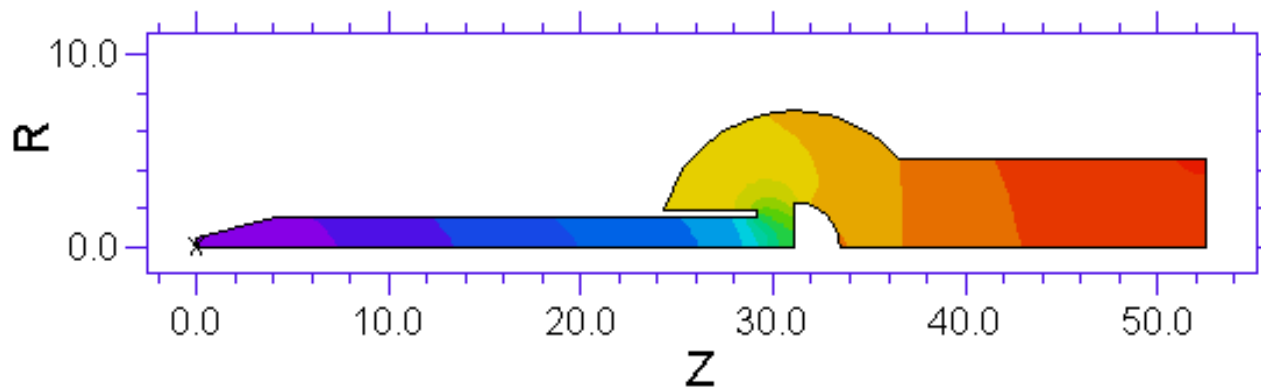
Boundary Conditions

- Flow is developed at entrance
- No-slip at surfaces
- Mass flux at surfaces due to recombination
- Outlet dimensionless pressure is zero
- Inlet dimensionless pressure is determined by checking the velocity profiles

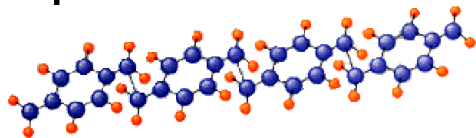
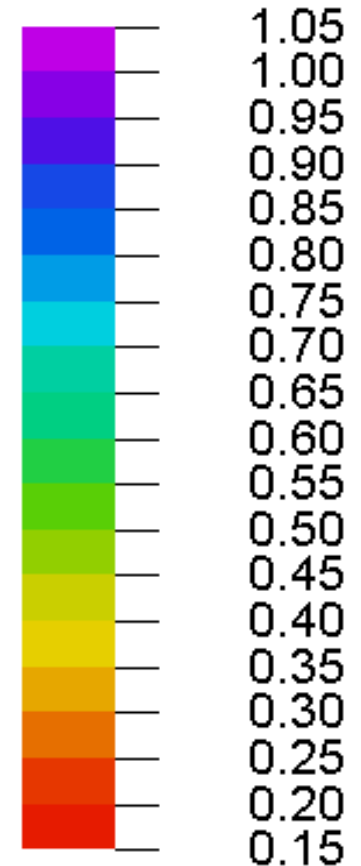


Atomic Oxygen Mole Fraction

Pressure = 1.0 Torr
Flow Rate = 125 sccm
100% Dissociation



X_O

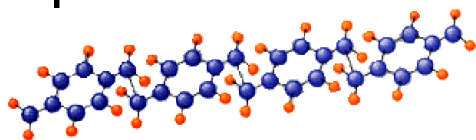
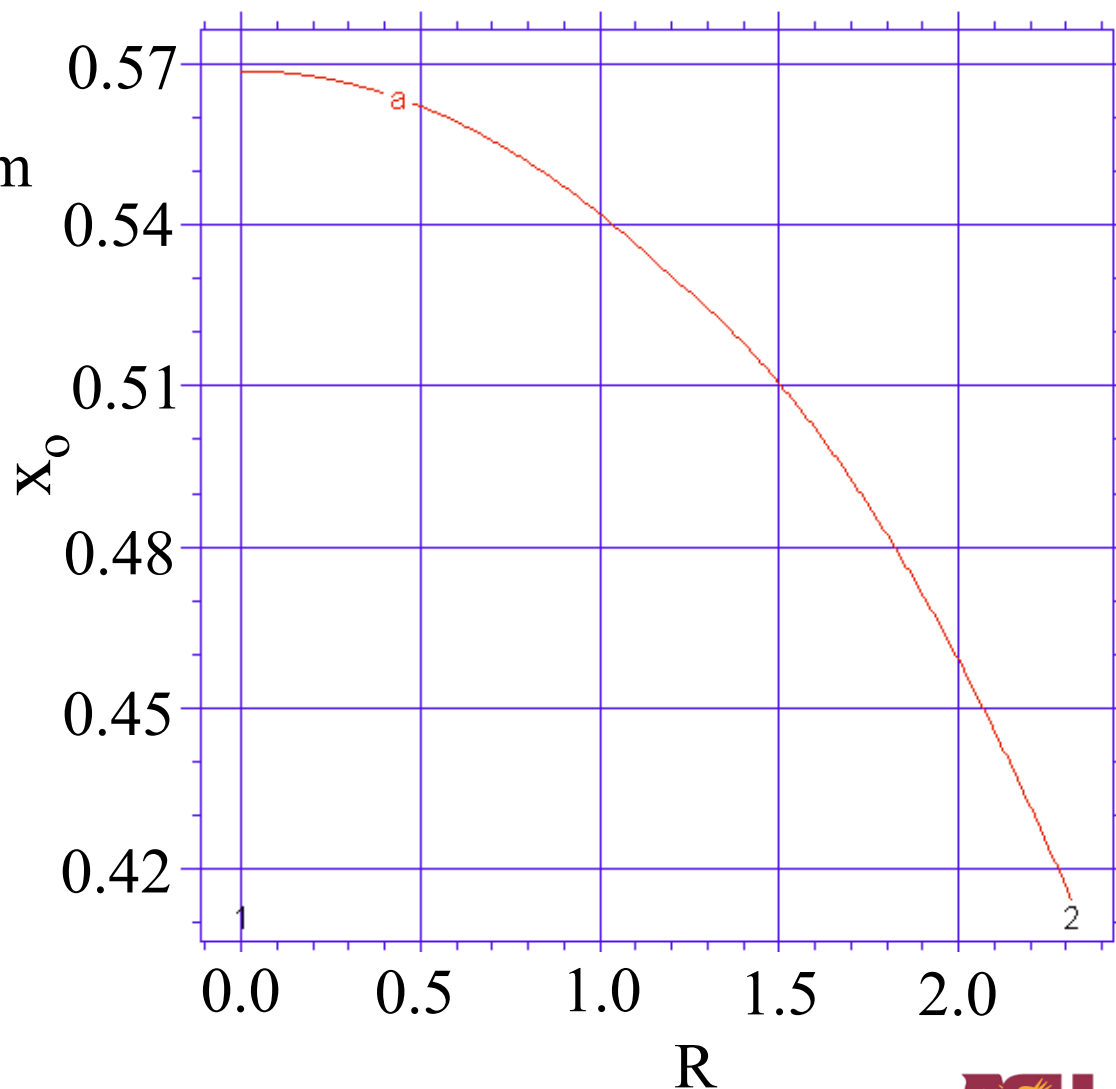


Atomic Oxygen Profile Along Sample

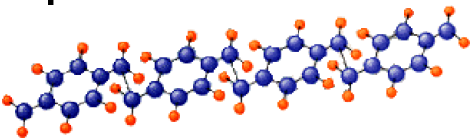
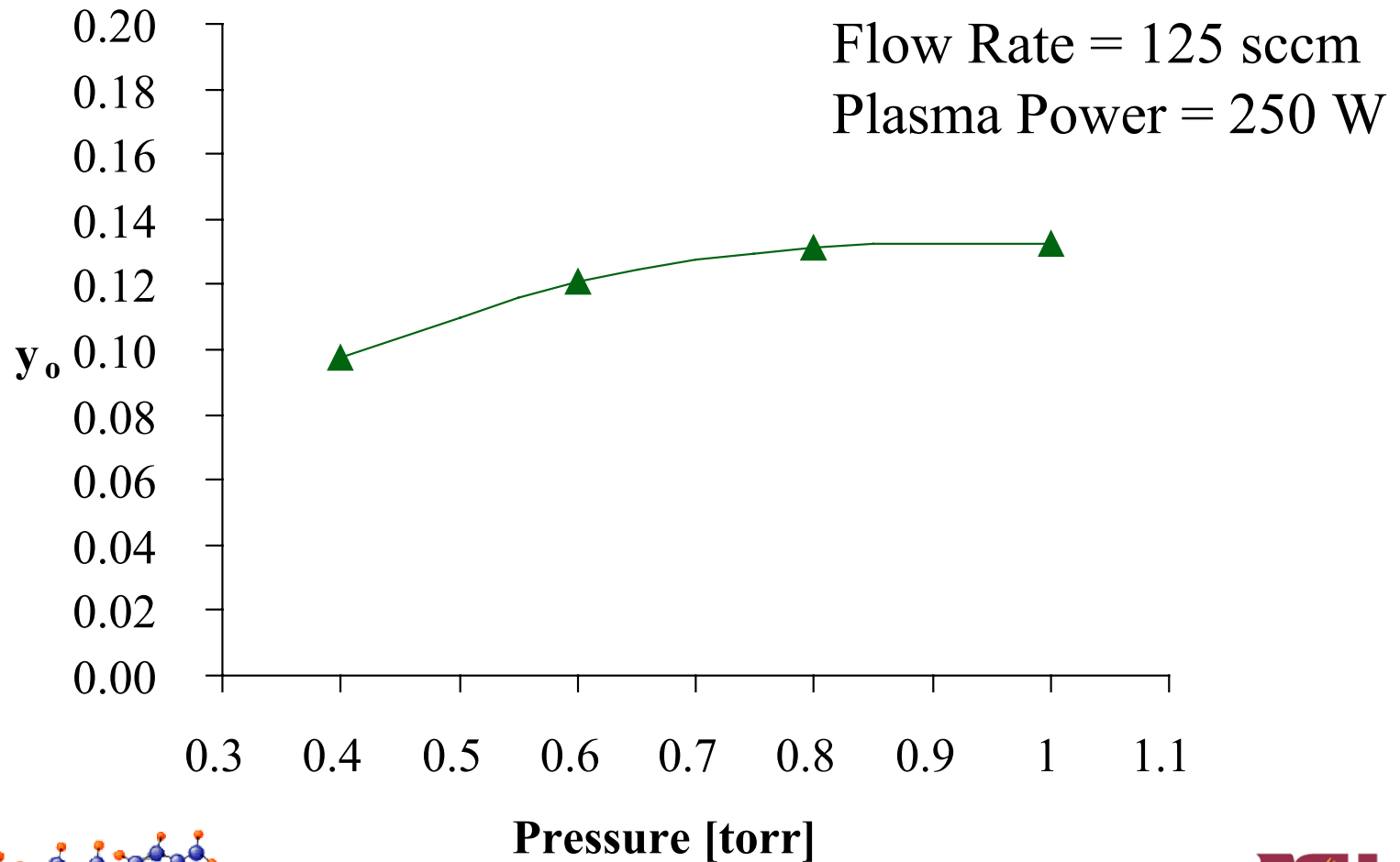
Pressure = 1.0 Torr

Flow Rate = 125 sccm

100% Dissociation



Results: Average Atomic Oxygen Mole Fraction on Sample as a Function of Pressure

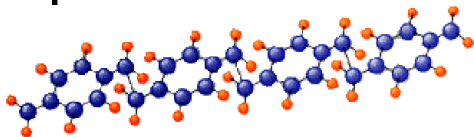


Etch Model

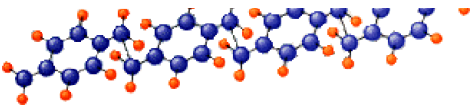
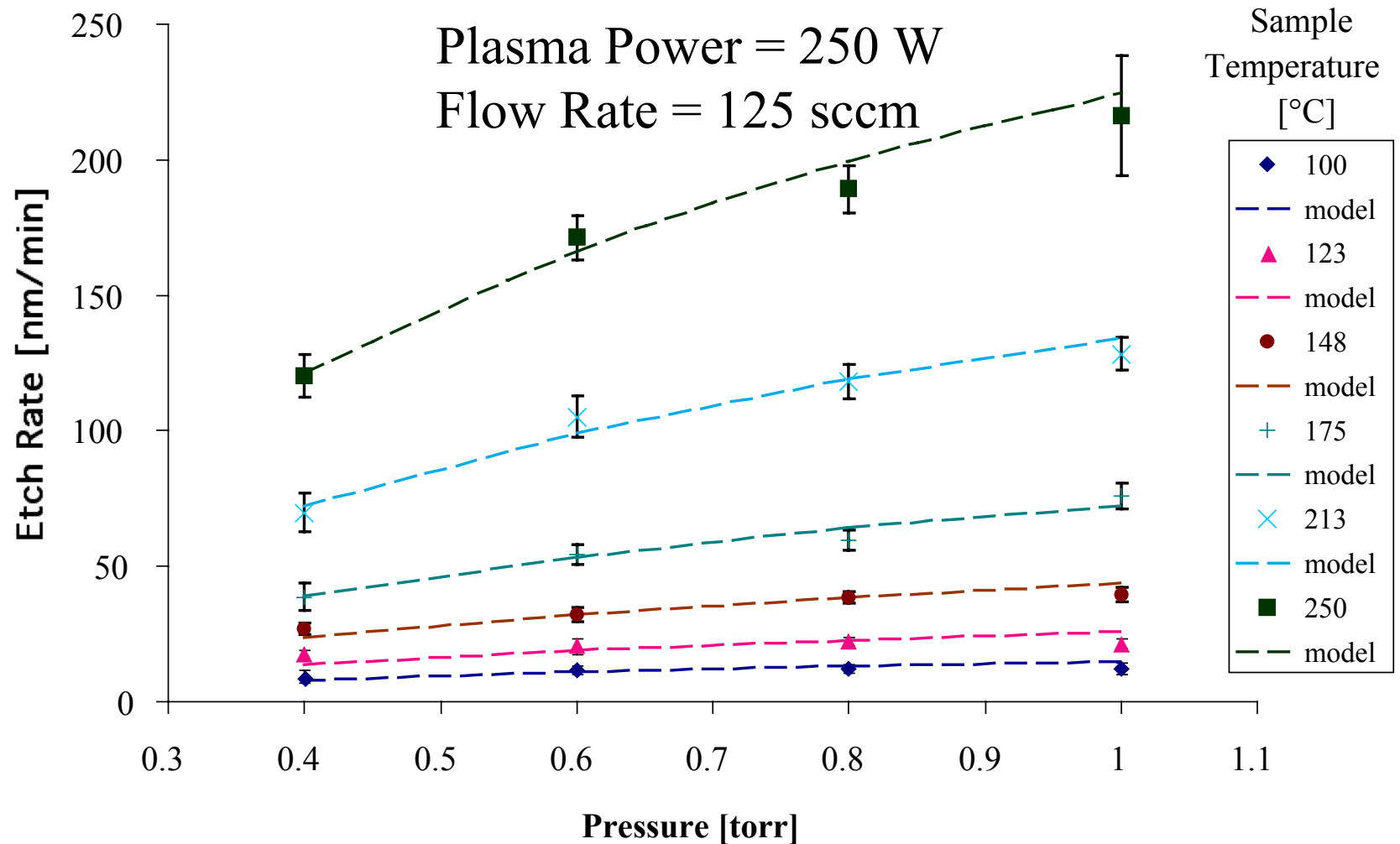
- Etch rate is dependent on oxygen atom concentration

$$\text{Etch Rate} = k_o \exp(-E_a / RT) N^\alpha y_o^\alpha$$

- k_o is a pre-exponential factor from experiment
- E_a is the activation energy from experiment
- N is the gas density
- y_o is the atomic oxygen mole fraction
- α is the reaction order

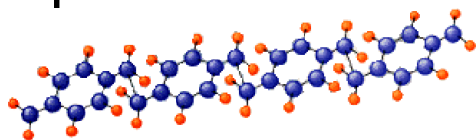
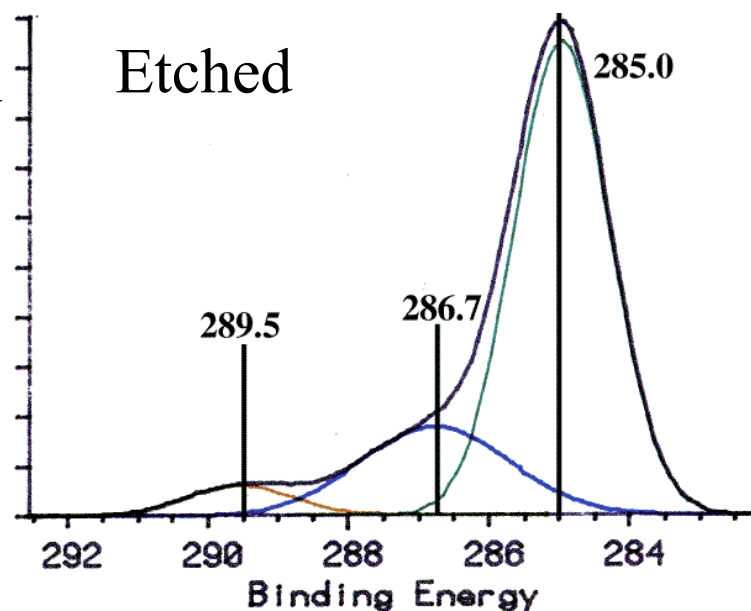
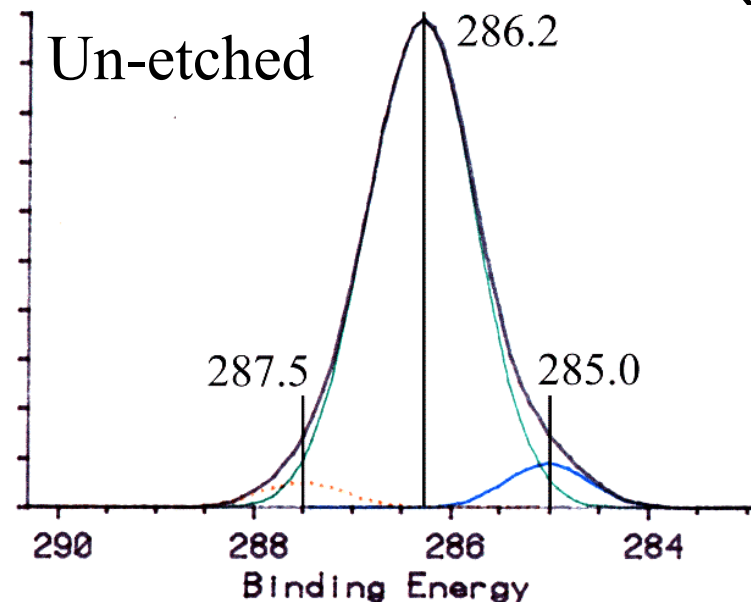


Comparison of Model and Experiments for $\alpha=0.5$

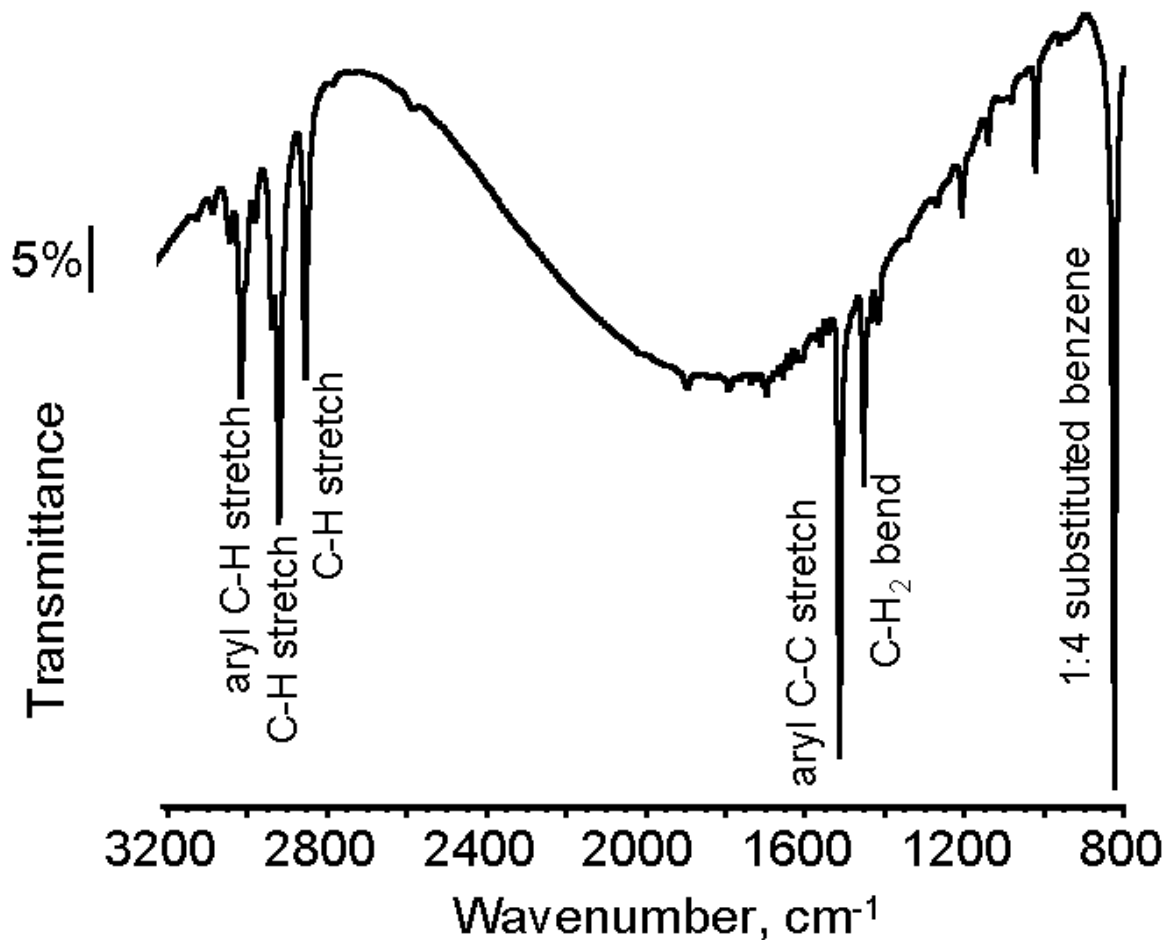


XPS Analysis

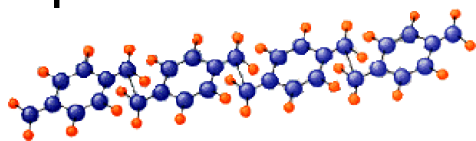
- Peak identification
 - 285.0 saturated carbon
 - 286.2-286.7 aromatic carbon
 - 287.5 oxygen contamination
 - 289.5 carboxylic acid
- Post-etch XPS shows the ratio of aromatic carbon to saturated carbon has been reduced
- Relative ratio information gives evidence of mechanism pathway



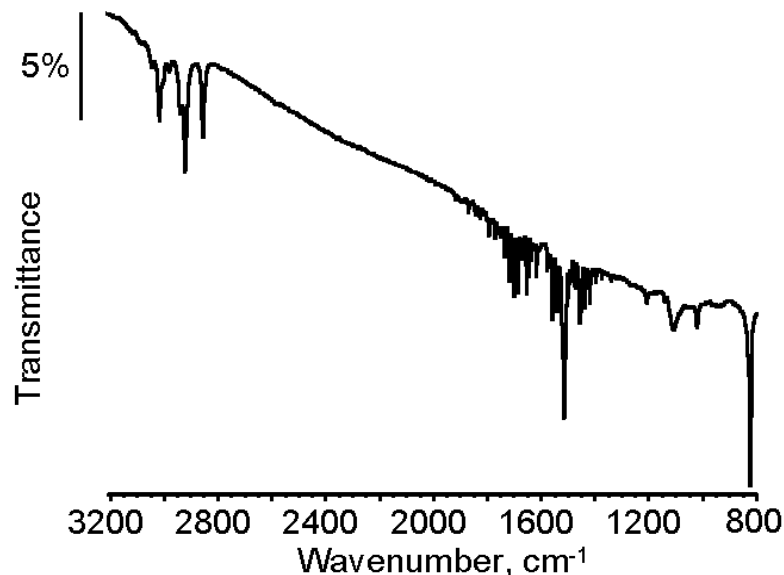
Infrared Analysis



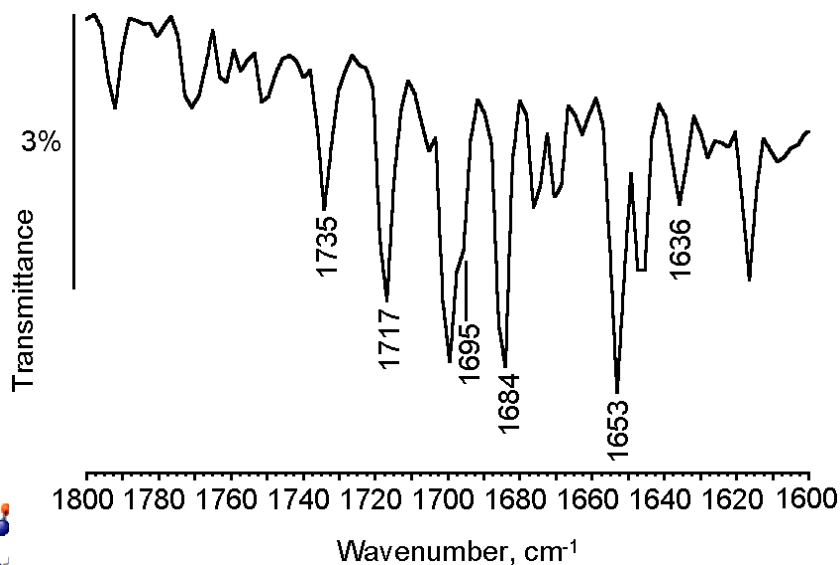
Parylene-n IR spectrum



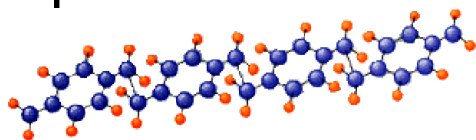
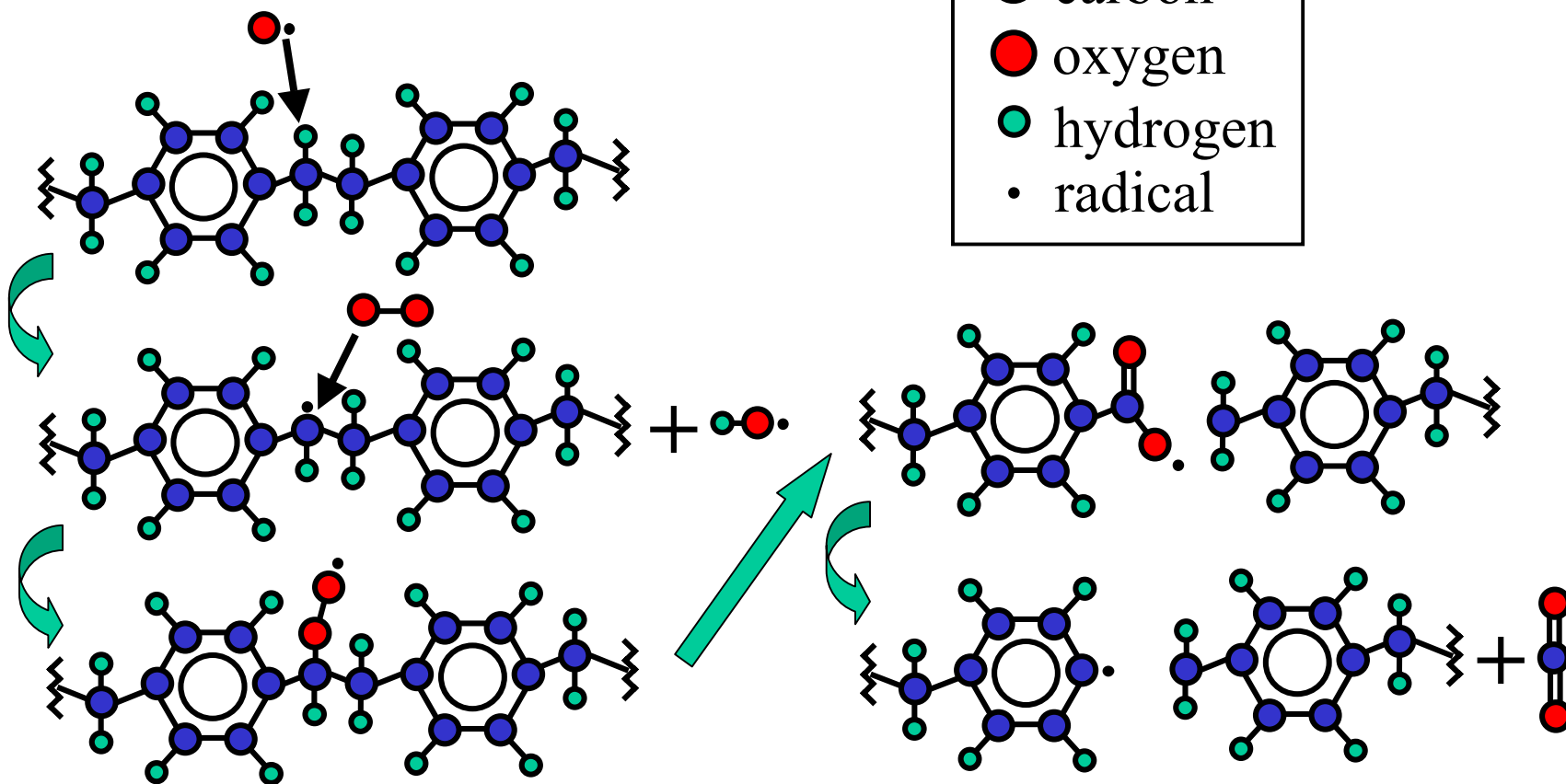
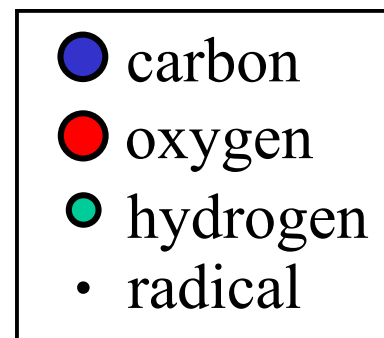
IR of Etched Sample



- IR spectrum of etched sample shows evidence of carbonyl formation
- The evidence being new absorption peaks around 1700 cm⁻¹

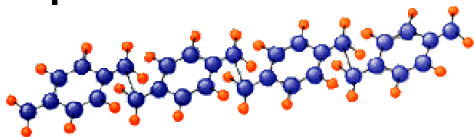


Possible Etching Mechanism



Conclusions

- Fundamental model for generation, transport and reaction in microwave system developed and validated
- Preliminary data suggests etch rate reaction order is 0.5 in oxygen atoms at conditions studied
- XPS and IR suggest carbonyl formation on the surface is one of the steps of the etching mechanism



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- Paratech, Inc. for supplying parylene-N coated wafers

